A photograph of a semi-industrial plant. In the center, a burner is lit, producing a bright orange flame. The surrounding environment is dark and filled with various mechanical components, pipes, and structures. The text is overlaid on the top half of the image.

Retrofitting oxy-fuel technology in a semi-industrial plant: flame characteristics and NOX production from a low NOX burner fed with natural gas

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D. Cumbo, J. Brunetti, N. Rossi *ENEL*

33rd International Symposium on Combustion

Introduction

The “Friendly Coal” project is funded by the EU within the framework “Research Fund for Coal and Steel”. The partners of the project are: ENEL, Technische Universität München (TUM), Austrian Energy and Environment (AEE), Technical University of Denmark (DTU), Technische Universität of Graz (TUG).

This presentation will show the results of the first phase of the experimental programme of this project; within this phase IFRF was in charge of the in-flame measurements

The objective of the experimentation is to run experiments with the existing low-NO_x burner in order to obtain a characterization of the combustion process with oxygen and recycled flue gas, with both natural gas and coal as fuels, and to produce data for computer modeling validation.



Experimental Setup

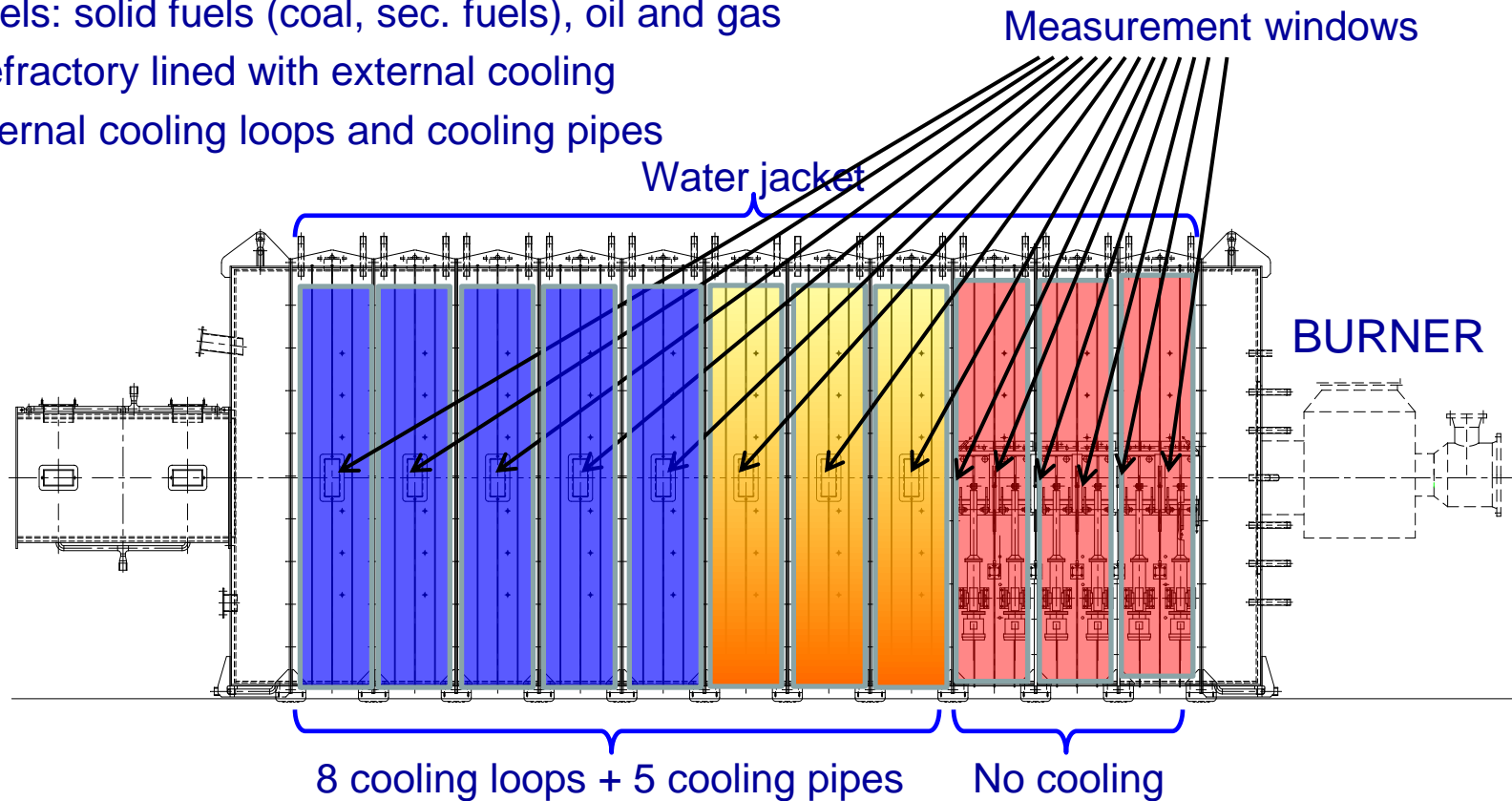
- The furnace
- The burner
- Modifications of the plant for oxy-combustion
- Measurements probes



The furnace

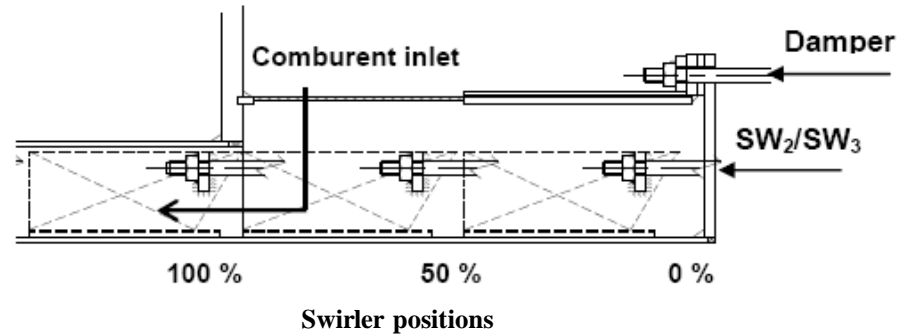
FOSPER (FOrnace SPERimentale – Experimental Furnace) is a replica of the former IFRF furnace number 1

- Dimensions: 2 m x 2 m x 6,25 m
- Fuels: solid fuels (coal, sec. fuels), oil and gas
- Refractory lined with external cooling
- Internal cooling loops and cooling pipes

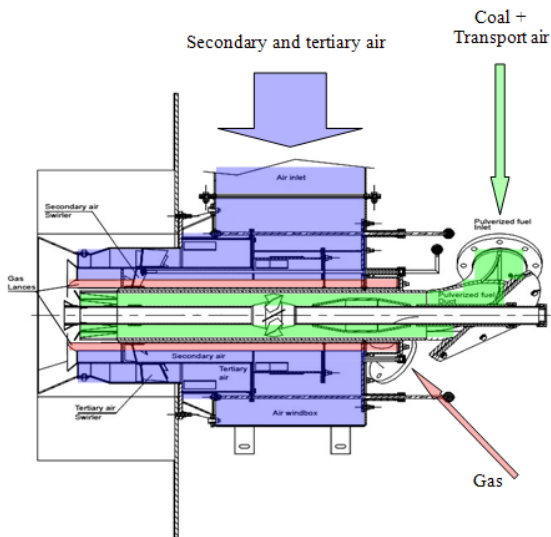


TEA-C Burner

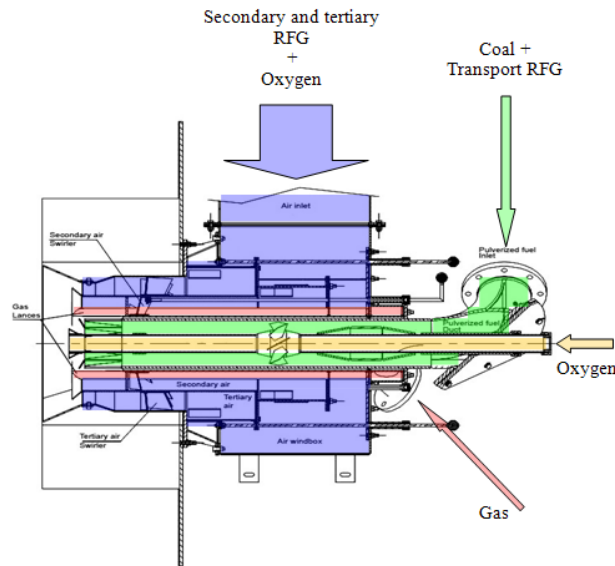
Low-NO_x Burner
 Secondary and tertiary air with independent swirler
 Fuels: NG, oil, coal



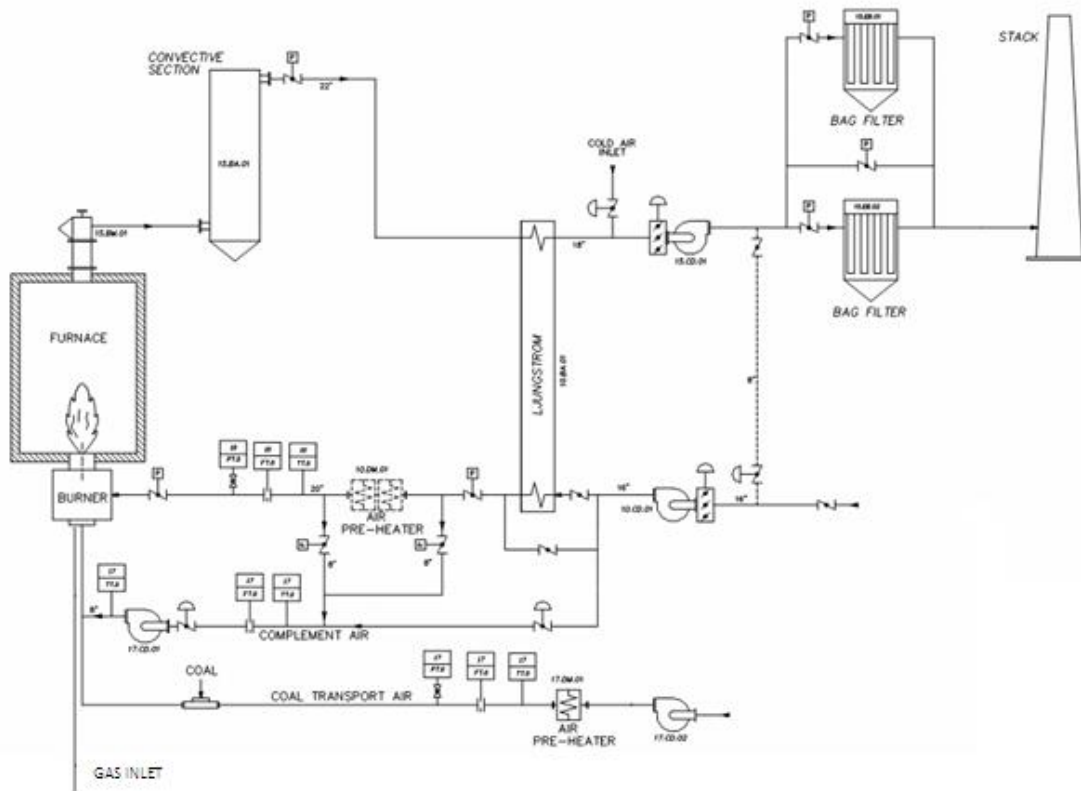
Conventional combustion



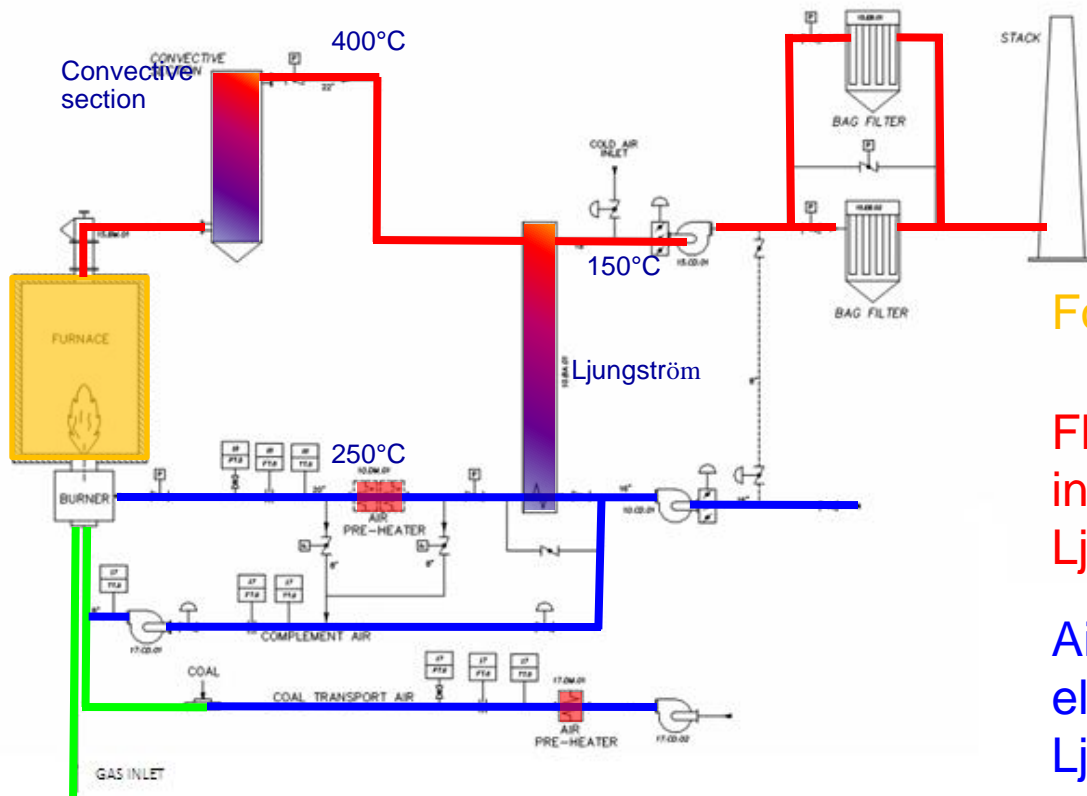
Oxy-combustion with RFG



Plant scheme for conventional combustion



Plant scheme for conventional combustion



Fo.Sper. : combustion chamber

Flue gas line: the FG is cooled down in the convective section and by the Ljungström heat exchanger

Air lines: the air is heated up by two electrical pre-heaters and by the Ljungström

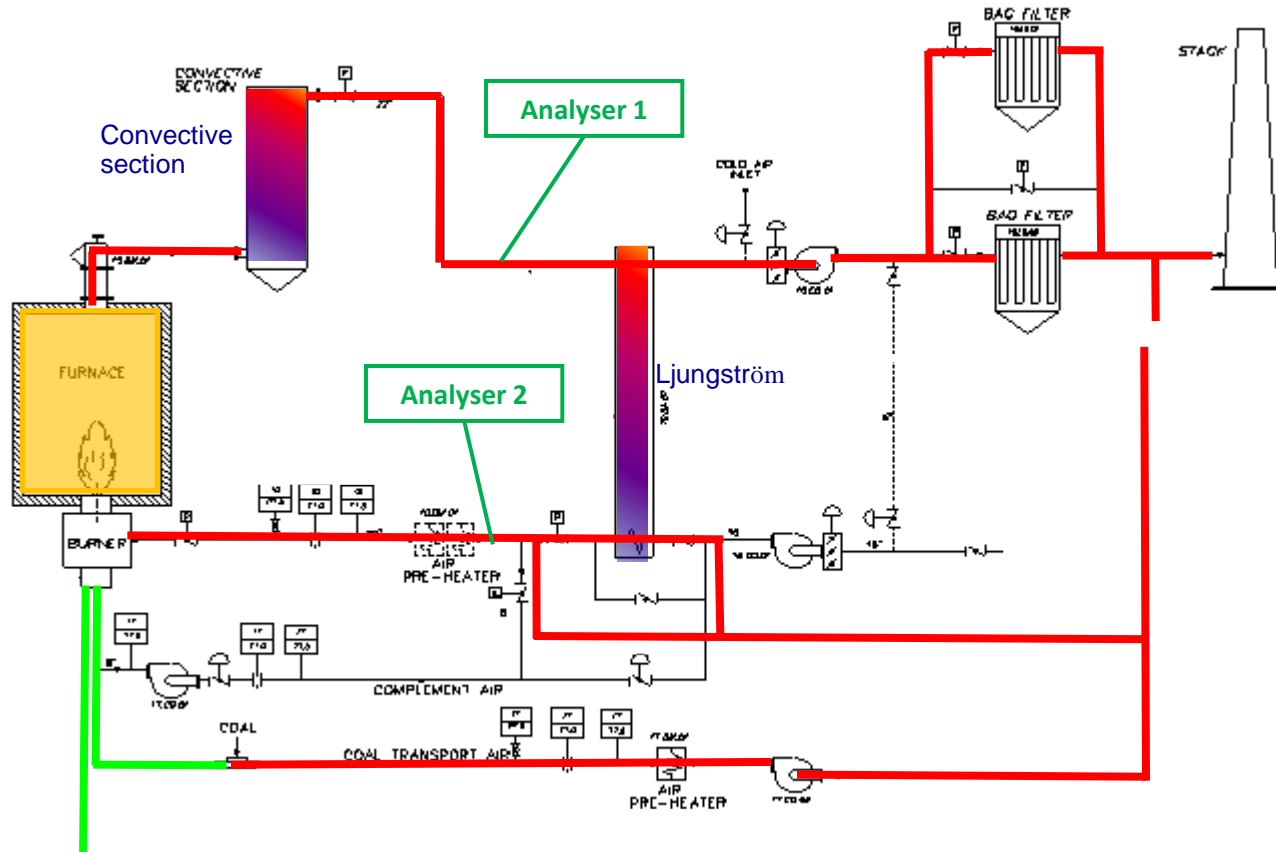
Fuel lines: for natural gas and coal



Plant scheme for oxy – combustion

Blu lines: oxygen injection

Pink lines: recycled flue gas



Measurements probes

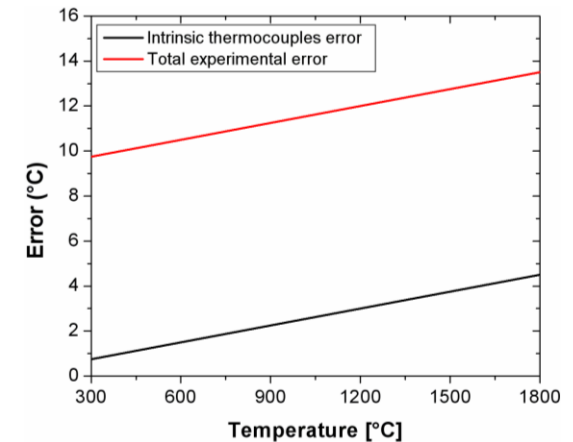
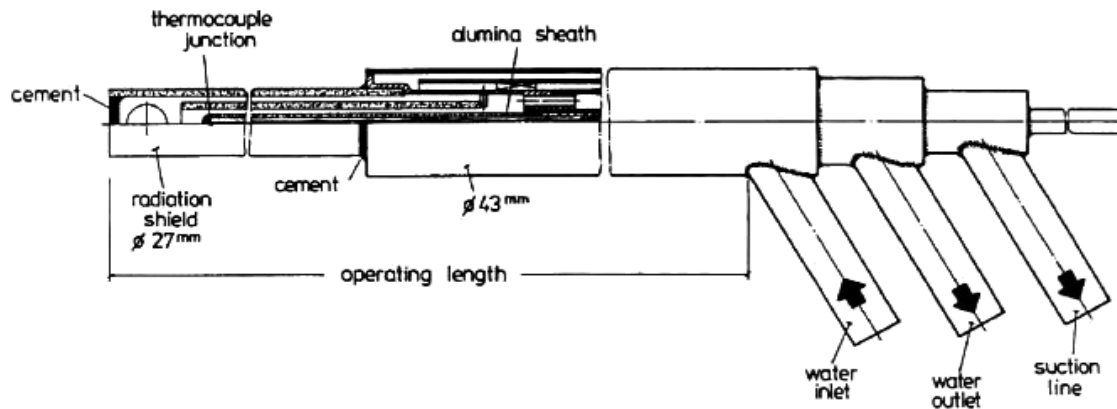
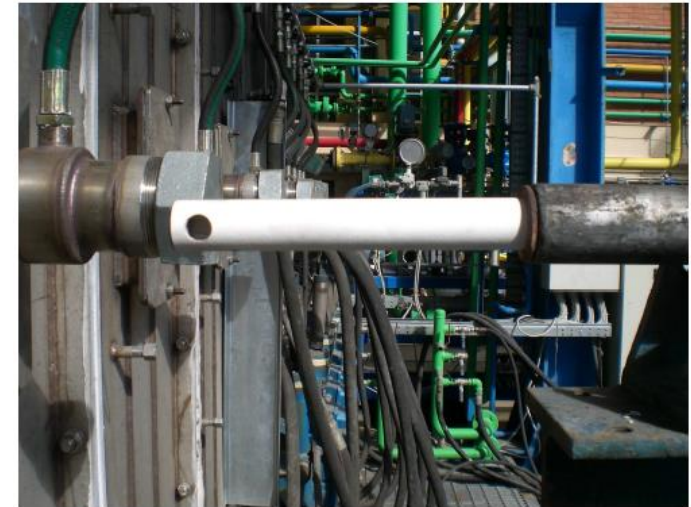


Water cooled suction pyrometer

In the standard suction pyrometer a platinum-rhodium thermocouple, protected from chemical attack by a sintered alumina sheath, is surrounded by two concentric radiation shields.

The gases are drawn between the shields and over the sheath with high velocity so that the equilibrium thermocouple temperature is nearly that of gases without the need for correction.

Max temperature: thermocouple S ~ 1750°C
thermocouple B ~ 1820°C
ceramic shield (Alsint 99.7%) ~ 2050°C



Intrinsic error for B and S thermocouples and total experimental error

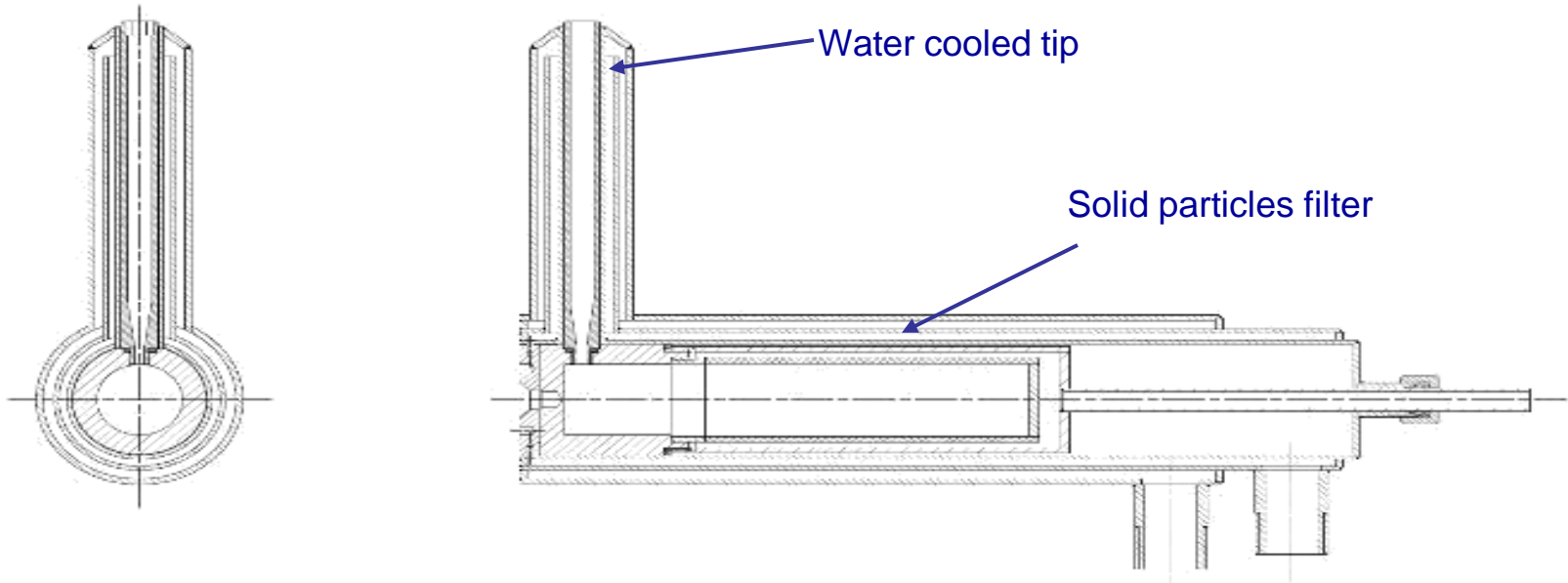


Gas/solid sampling probe

- Gas species concentration profiles (O_2 , CO_2 , NO , CO)
- Solid sampling

The accuracy of the analyzers is normally below 1ppm but the total error of the data is conditioned by the method of sampling.

A study about experimental errors introduced with different sampling techniques is currently ongoing at the IFRF.

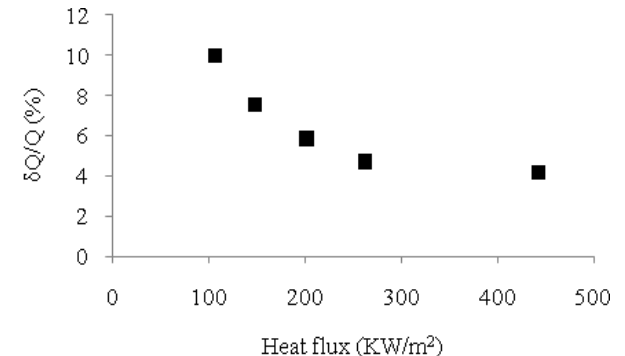
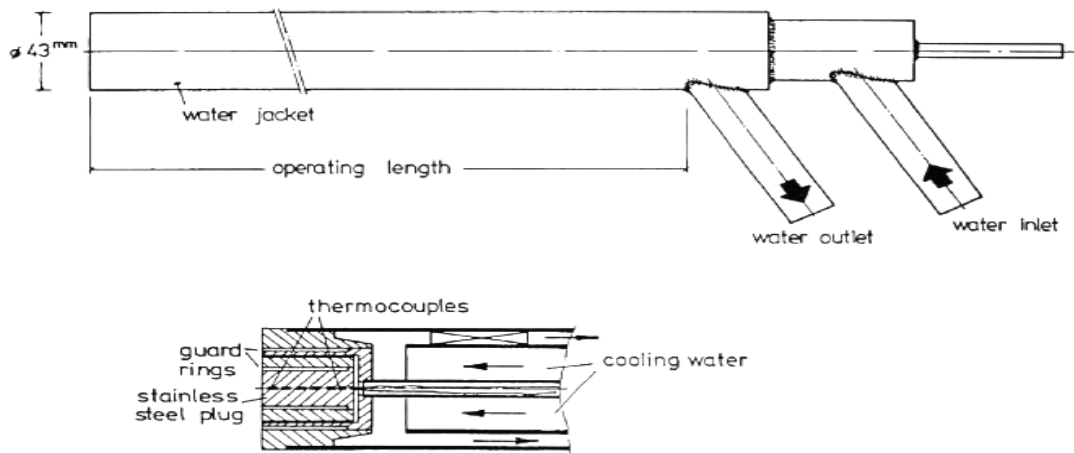


Total heat flux meter

The IFRF heat flux meter is designed to measure the total heat transfer (conduction + convection + radiation) from the combusting flow to its front surface.

The principle of the total heat flux measurement is based on the measurement of the temperature gradient through a steel plug of known thermal conductivity mounted at the tip of the probe.

The response time for this instrument is in order of 10 minutes.



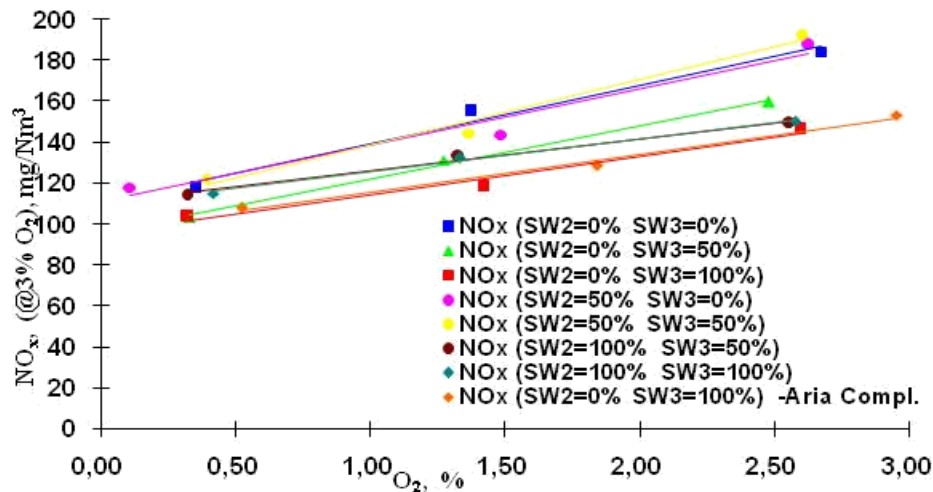
Relative error in the heat flux measurements

Burner settings

The driving guidelines for the assessment of the best settings were the following:

- **Flame stability.**
- **Minimize NO_x emissions**
- **Maximize flue gas CO₂ concentration.**
- **Comparison needs (heat transfer)**

In **conventional combustion** the best setting of the swirlers was the one that produced less NO_x emissions

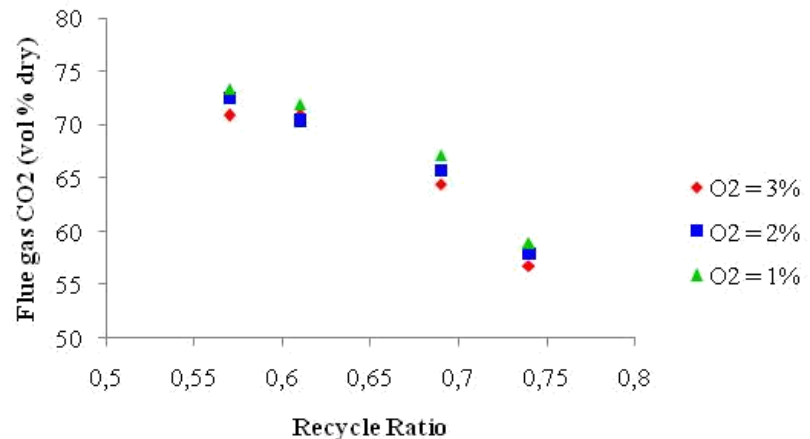
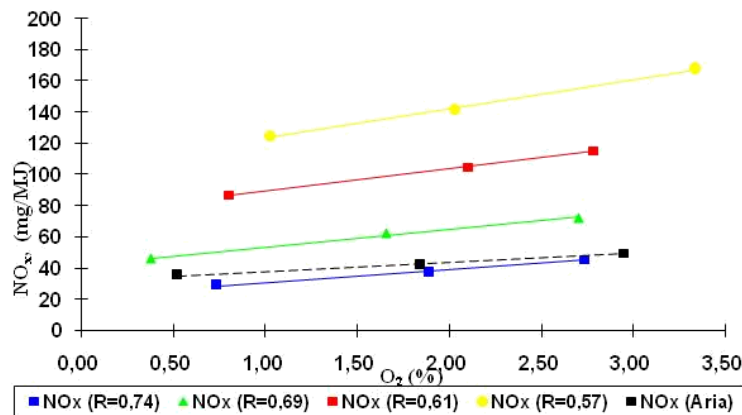


Burner settings

The driving guidelines for the assessment of the best settings were the following:

- **Flame stability.**
- **Minimize NO_x emissions**
- **Maximize flue gas CO₂ concentration.**
- **Comparison needs (heat transfer)**

In **oxy-combustion** the best setting of the swirlers was the same used for conventional combustion and the optimum recycle ratio was the best compromise between NO_x and CO₂ emissions



In flame measurements

Temperature and chemical species (O_2 , CO_2 , NO_x , CO) in-flame measurements were carried out in the following conditions:

- **Conventional gas-air combustion**
- **Natural gas with pure oxygen and recycled flue gas combustion, $R=0.61$ and $R=0.69$**
- **Conventional coal-air combustion**
- **Coal with pure oxygen and recycled flue gas combustion, $R=0.61$**



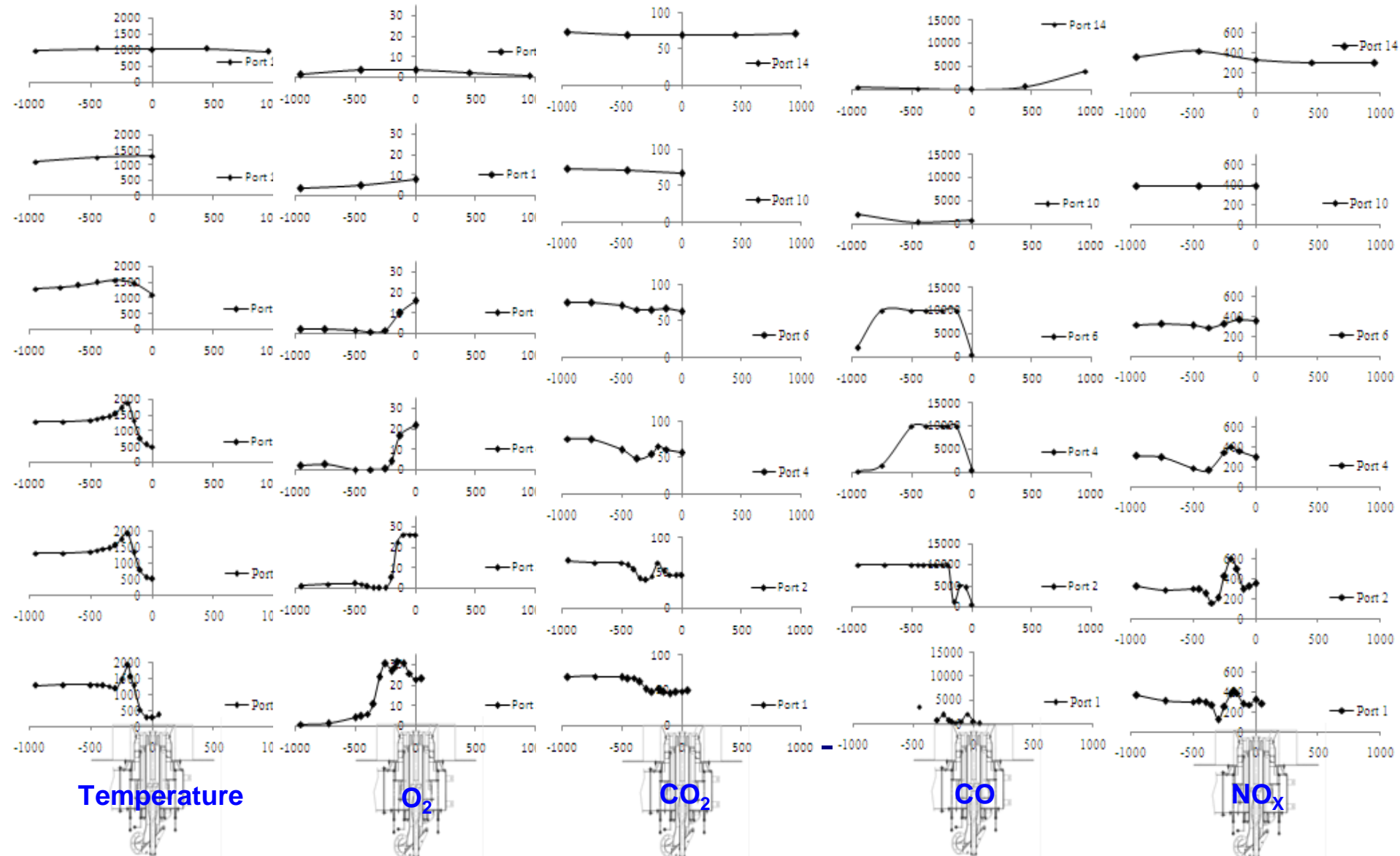
Input-Output conditions

INPUT CONDITIONS					
	NATURAL GAS			COAL	
	AIR	OXY		AIR	OXY
Natural gas flowrate	272 Nm ³ /h	267 Nm ³ /h	265.9 Nm ³ /h	-	-
Coal flowrate	-	-	-	360 kg/h	360 kg/h
Primary air	538 kg/h	-	-	501.8 kg/h	-
Primary air temperature	149°C	-	-	77°C	-
Sec/tert air	2798 kg/h	-	-	3100 kg/h	-
Sec/tert air temperature	251°C	-	-	250°C	-
Oxygen	-	729 kg/h	731.1 kg/h	-	718 kg/h
Primary RFG	-	700 kg/h	693.4 kg/h	-	700 kg/h
Sec/tert RFG	-	1447 kg/h	871 kg/h	-	1063 kg/h
Recycle ratio	-	0.69	0.61	-	0.61
Thermal input	2.5 MW _t	2.5 MW _t	2.5 MW _t	2.5 MW _t	2.5 MW _t

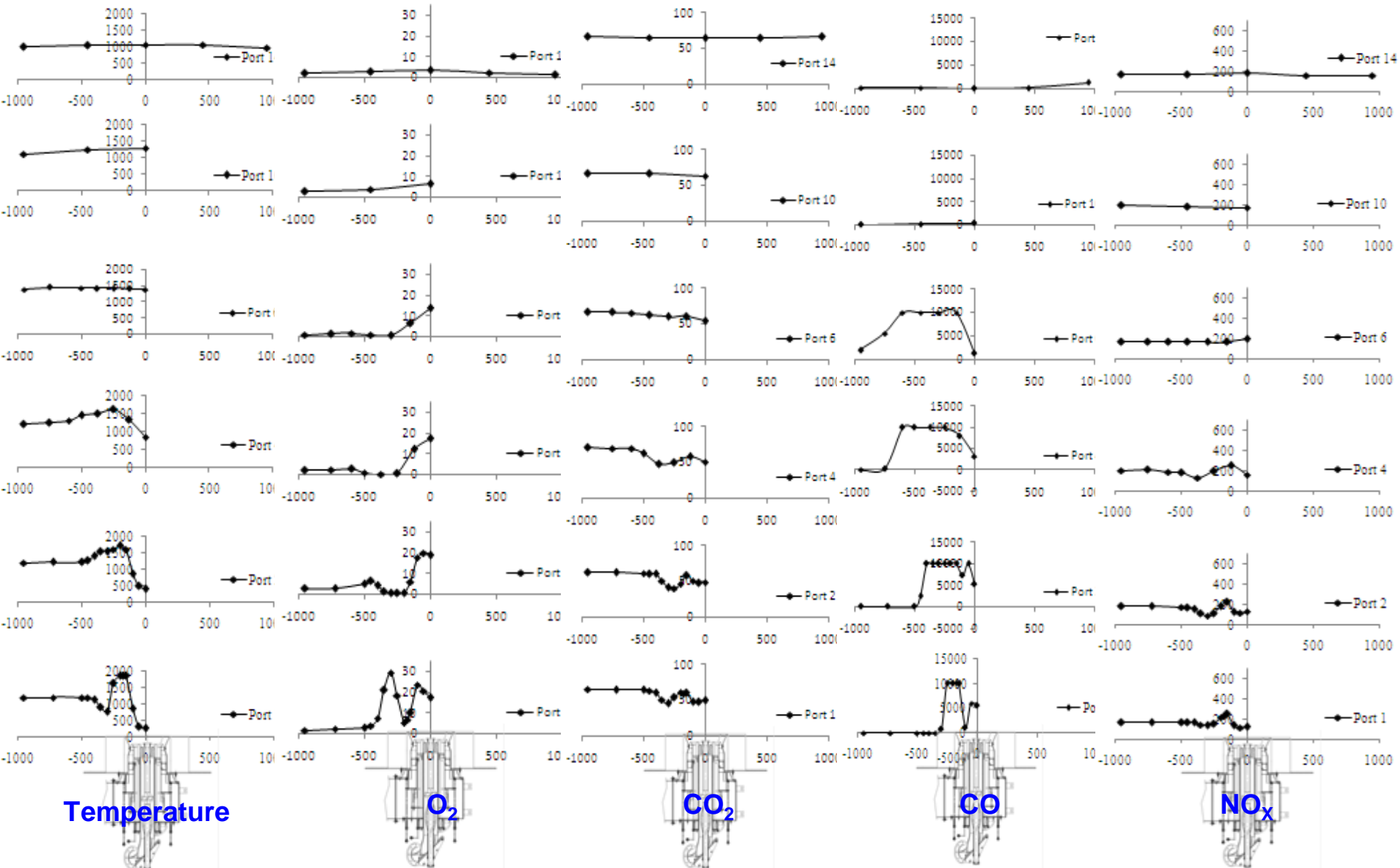
OUTPUT CONDITIONS					
	NATURAL GAS			COAL	
	AIR	OXY		AIR	OXY
Flue gas temperature	1100°C	1050°C	1025°C	1130°C	1250°C
Total heat extraction	1.115 MW	1.186 MW	1.28 MW	0.873 MW	0.93 MW
O ₂	1.9%	3.2%	3%	3.9 %	2.76 %
CO	-	11 ppm	12 ppm	0 ppm	19 ppm
CO ₂	10.8%	68.7 %	73.7%	14.57 %	76.22 %
NO _x	66 ppm	120 ppm	268 ppm	171 ppm	238 ppm
SO ₂	-	-	-	314 ppm	646 ppm



Measurements results: oxy-gas, $R=0.61$



Mesurements results: oxy-gas, R=0.69



Temperature

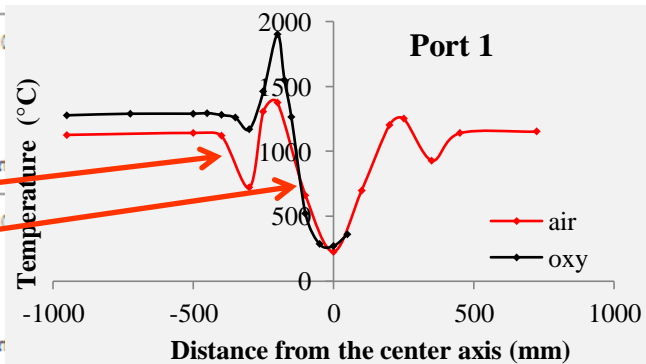
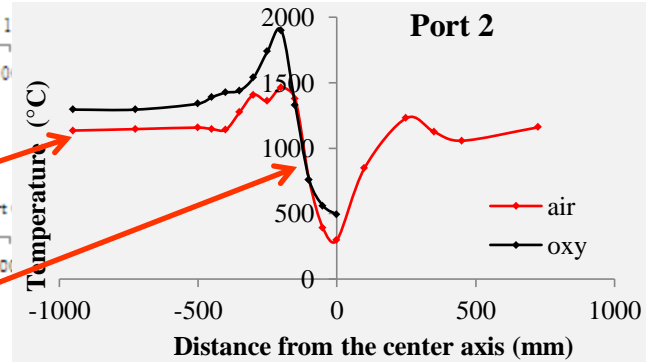
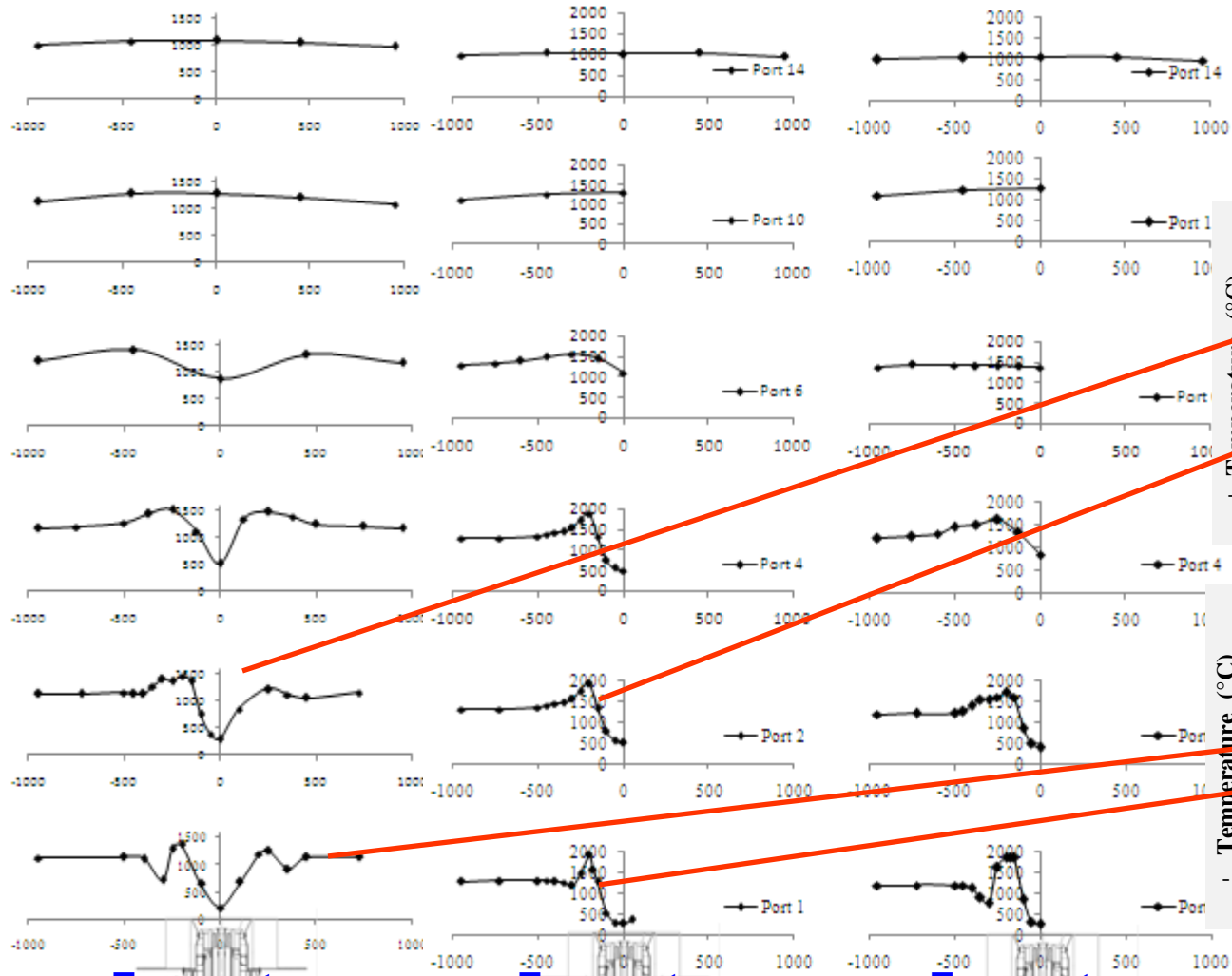
O₂

CO₂

CO

NO_x

Gas firing temperature comparison

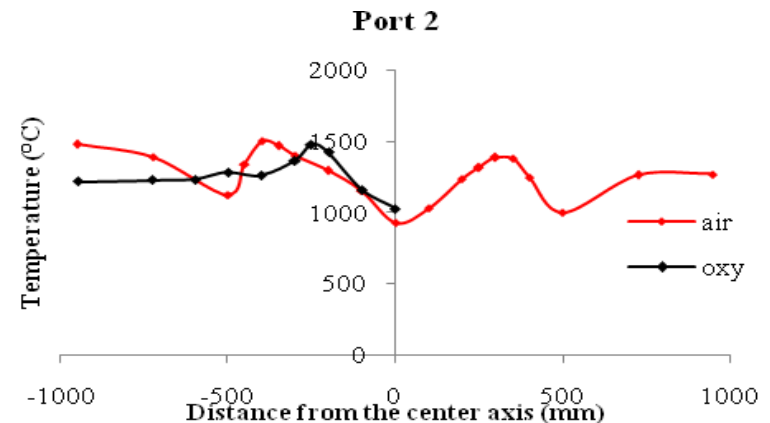
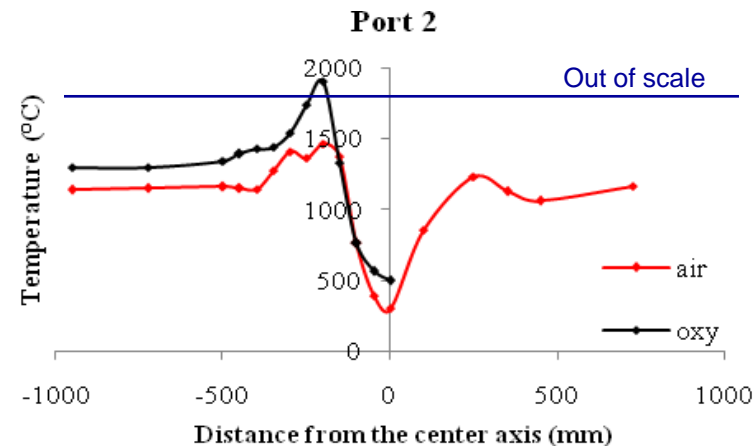
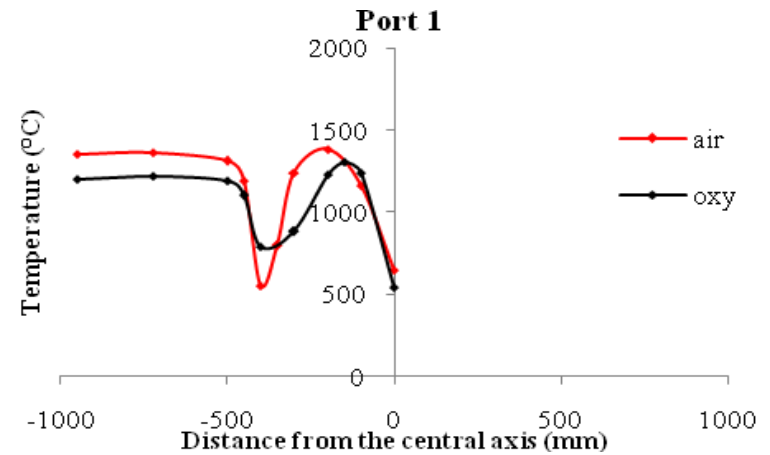
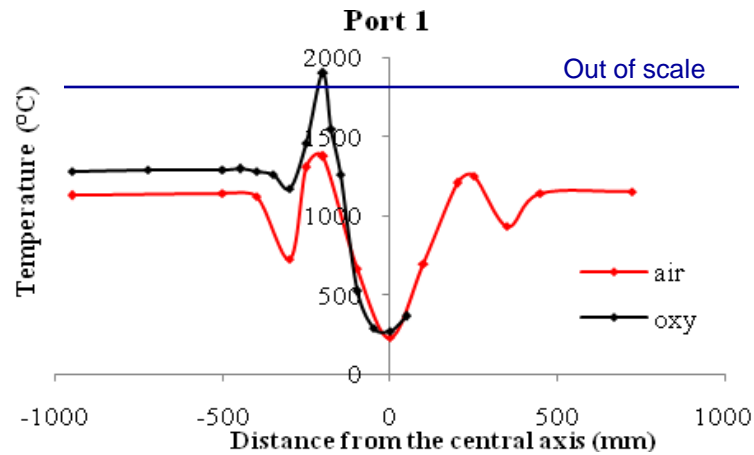


Temperature
Aria - gas

Temperature
oxy - gas $R=0.61$

Temperature
oxy - gas $R=0.69$

Air and oxy temperature comparison



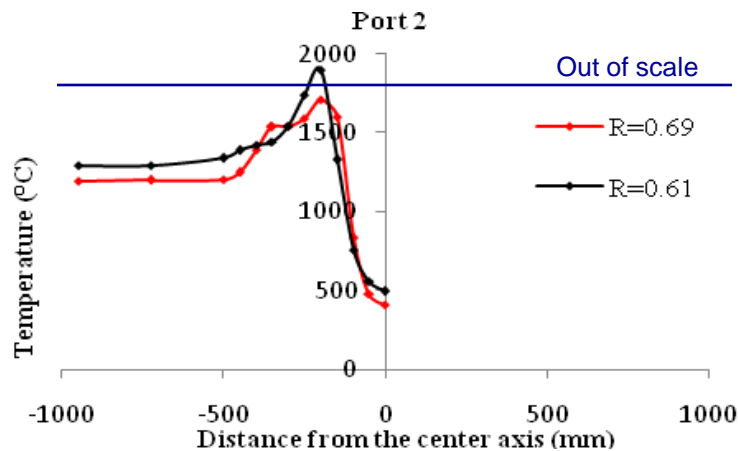
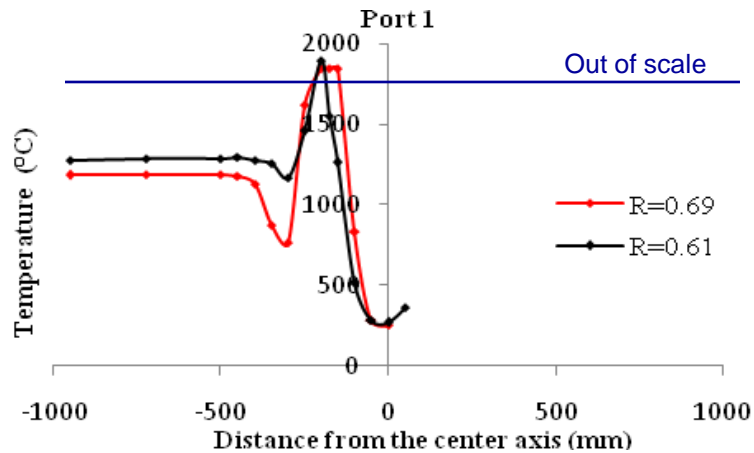
Gas firing

Coal firing

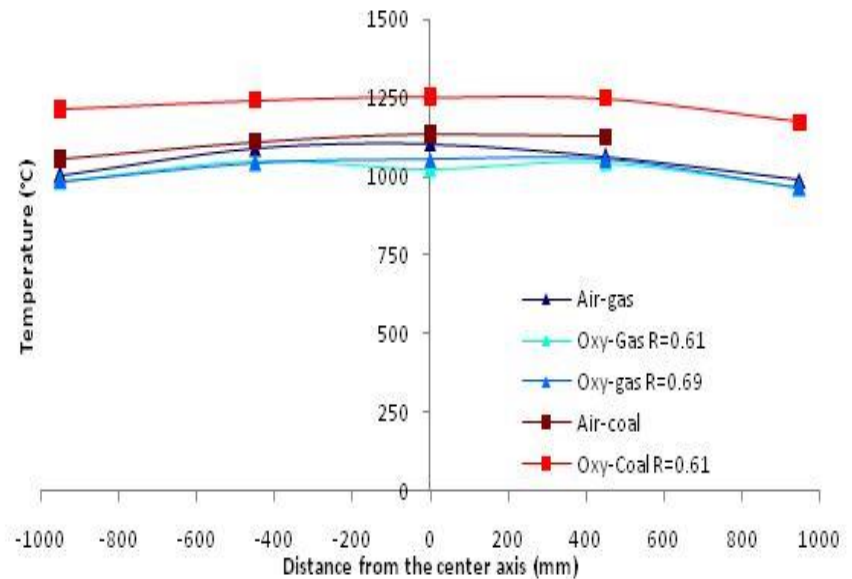


Temperature results

Effect of the recycle ratio



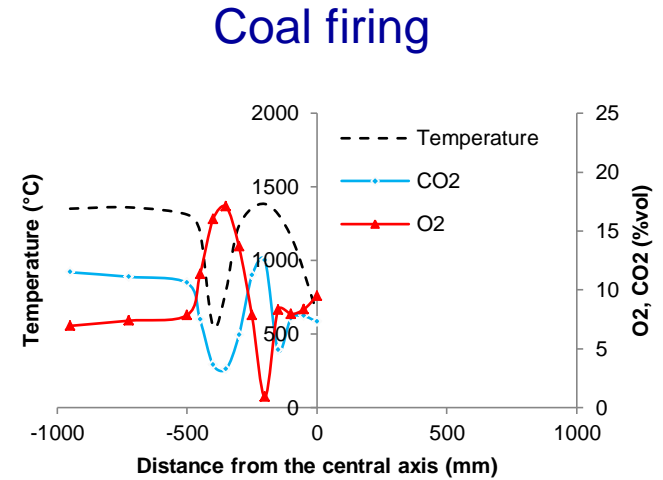
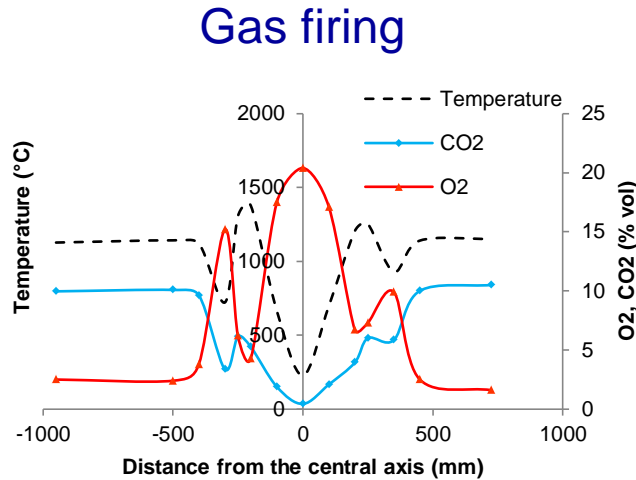
Temperature at the end of the furnace



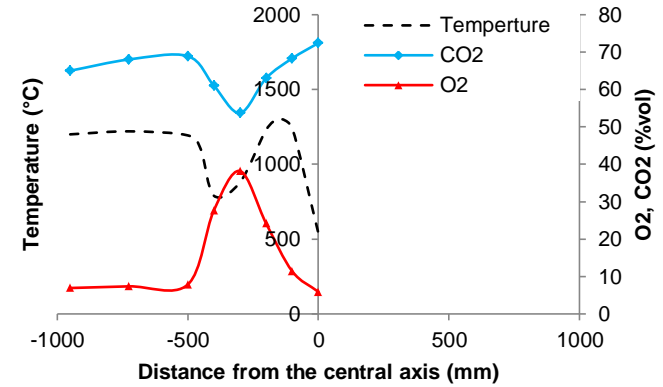
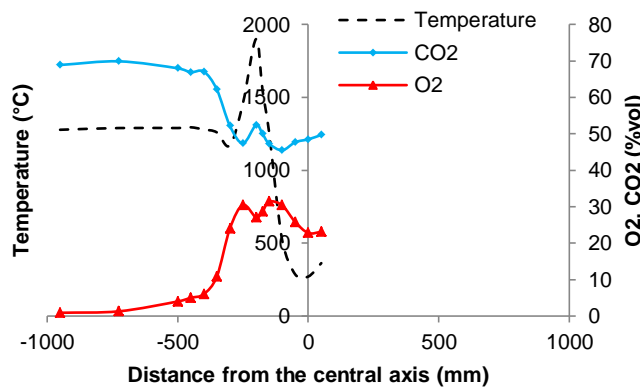
Chemical species

Gas composition profiles at the burner exit (port 1)

Conventional combustion



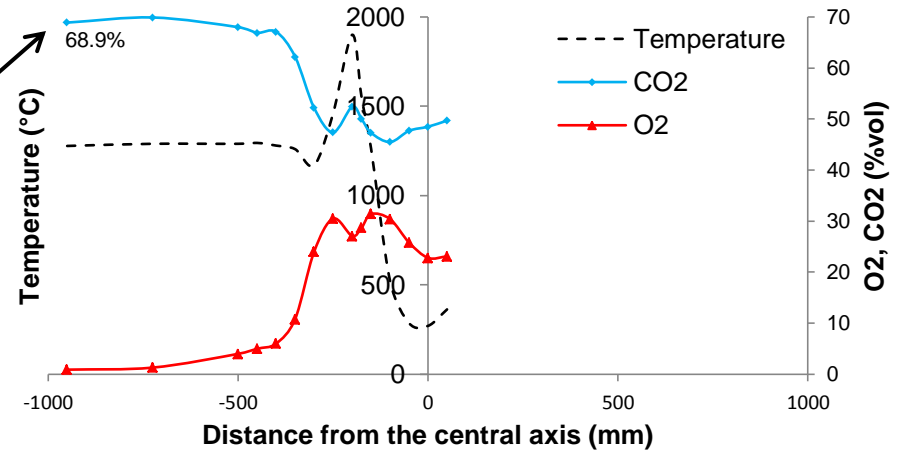
Oxy-combustion,
 $R=0.61$



External recirculation zone

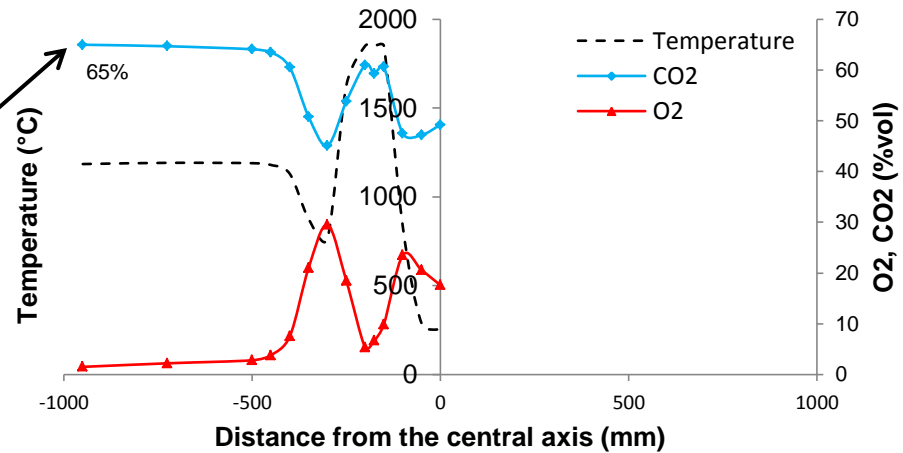
Output conditions

Recycle Ratio R	0.61
Temperature	927 °C
O ₂	3%
CO ₂	73.7%
NO _x	268 ppm
CO	12 ppm



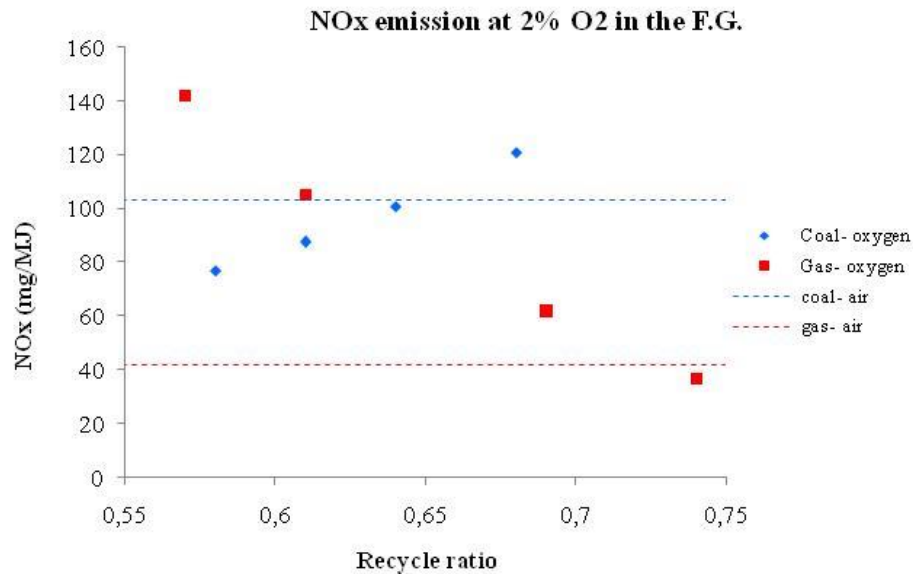
Output conditions

Recycle Ratio R	0.69
Temperature	919 °C
O ₂	3.2%
CO ₂	68.7%
NO _x	120 ppm
CO	11 ppm



NO_x emissions

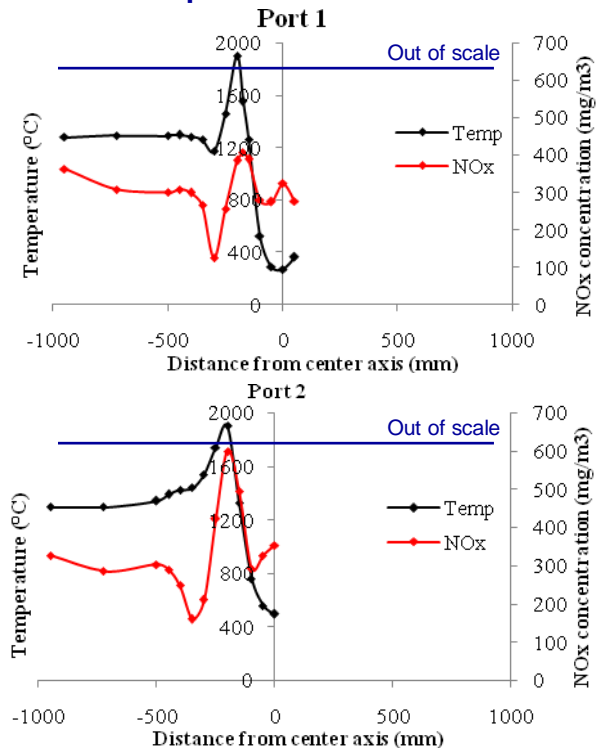
- NG-oxy combustion. The NO_x emission decreases as the recycle ratio increases. The emissions in oxy-combustion are generally higher than in conventional combustion
- Coal oxy-combustion. The NO_x emission increases as the recycle ratio increases. The emissions in oxy combustion are lower than conventional combustion for R<0.64.



NO_x emissions

Oxy-gas

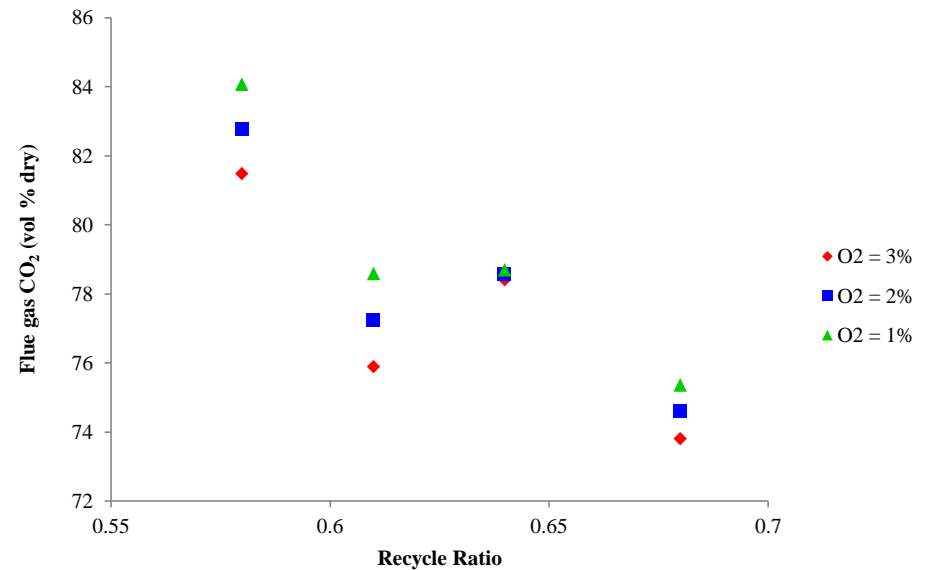
Thermal NO_x emissions predominant



Oxy-coal

Air-in leakage effect predominant

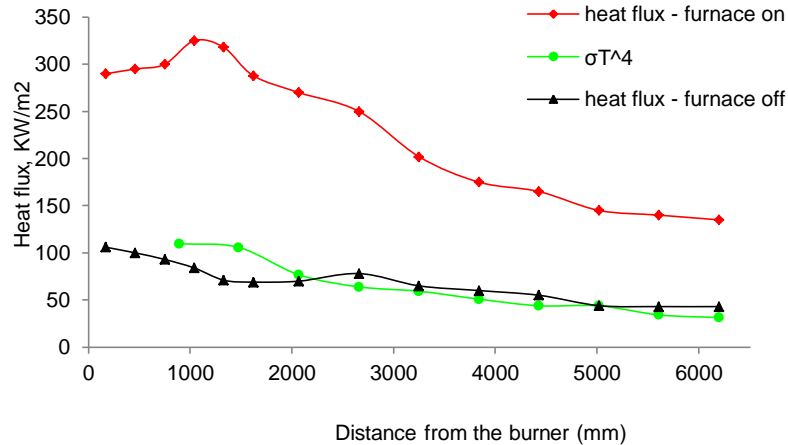
As the recycle ratio increase the air in-leakage in the system increase



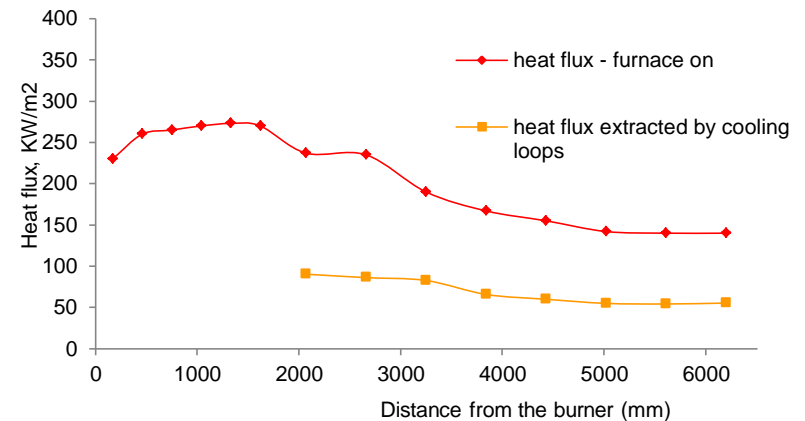
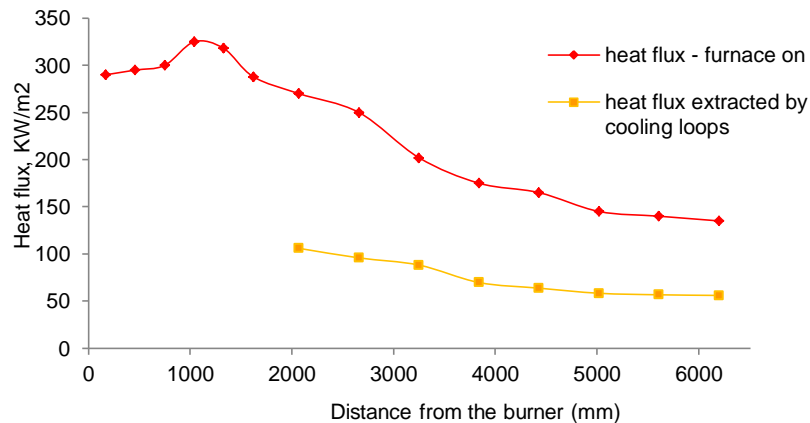
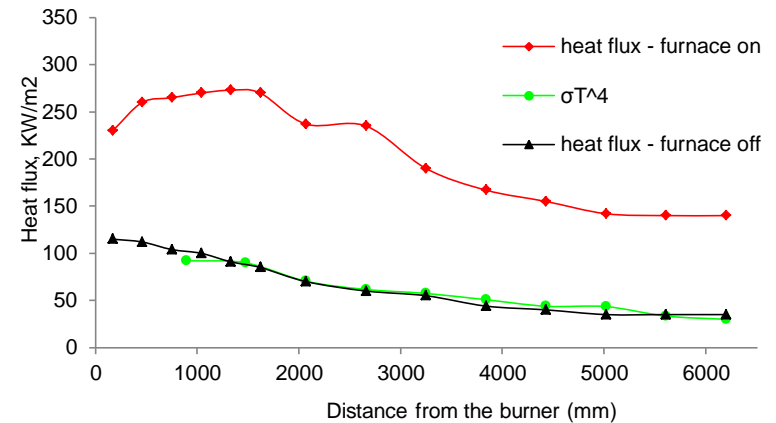
Total heat flux hitting the walls

Oxy-gas combustion

R=0.61



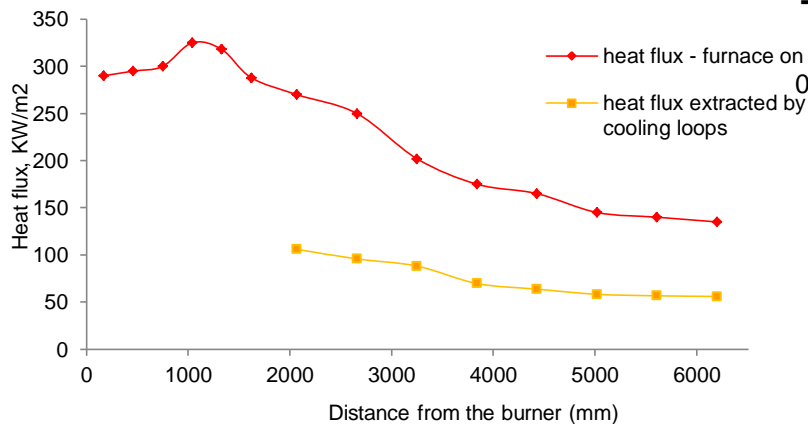
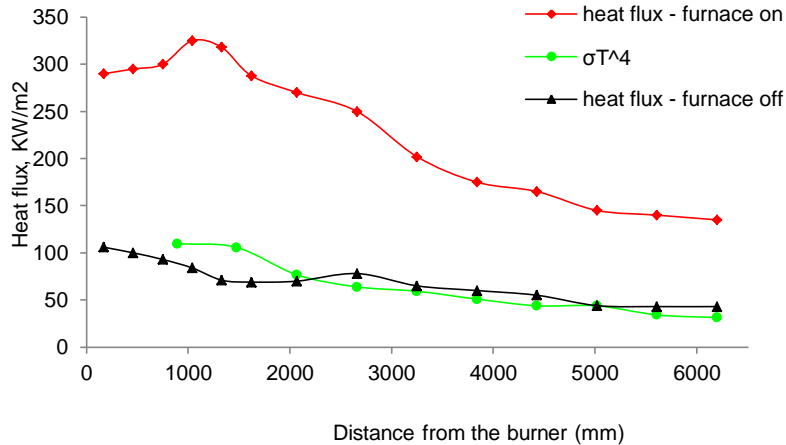
R=0.69



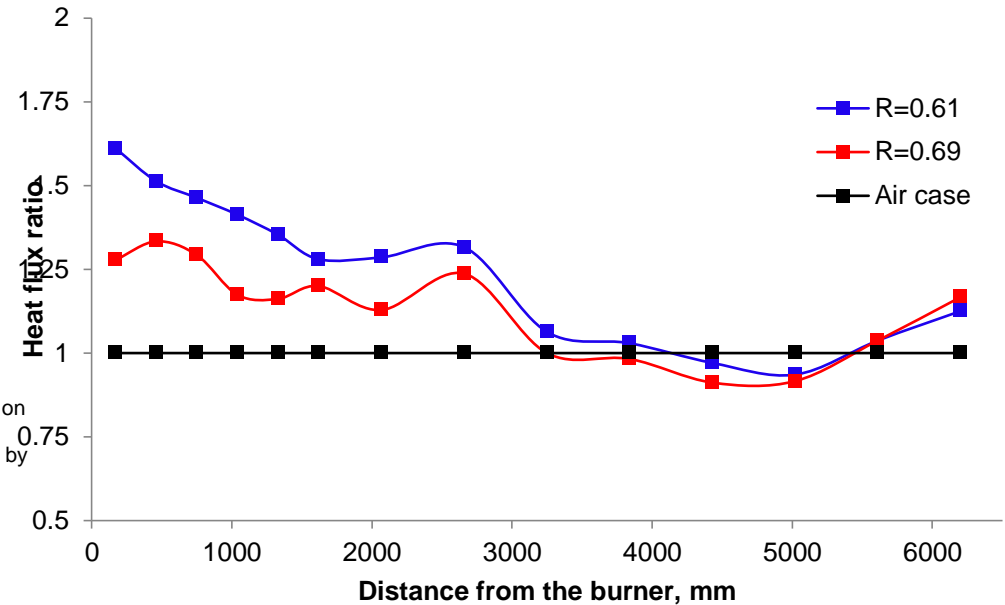
Total heat flux hitting the walls

Oxy-gas combustion

R=0.61



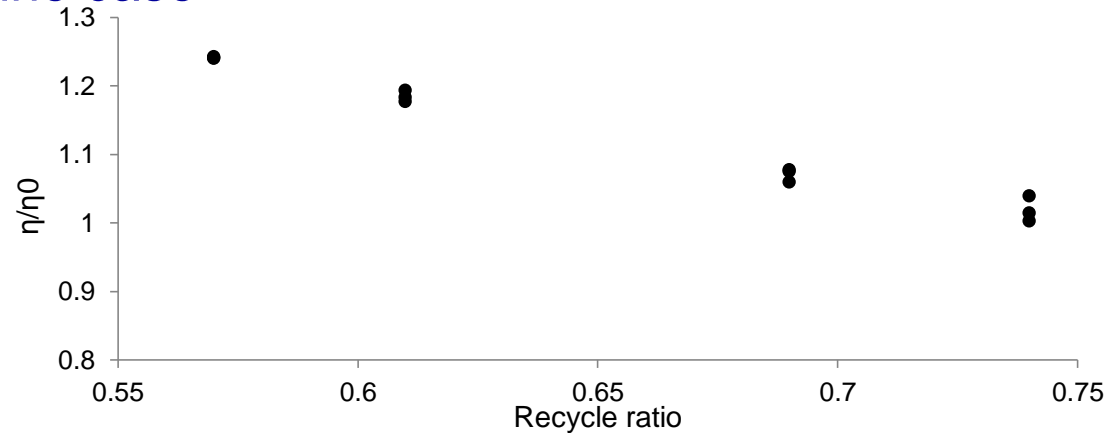
Heat flux oxy combustion/ heat flux baseline case



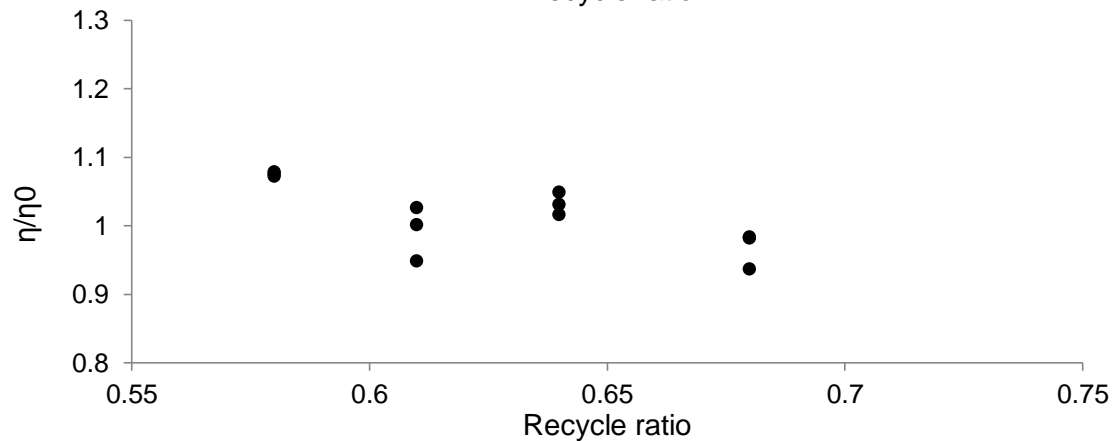
Heat transfer efficiency

Total heat extracted by cooling loops / total heat extracted by cooling loops in the baseline case

Oxy-gas



Oxy-coal



Conclusions (1)

- Modified FoSper plant is OK for oxy-combustion studies
- Important **air in-leakage** is present at high R
- The process of retrofitting the FOSPER rig was studied. Some of the issues arisen in this work can give a good indication about what would be the problems if an industrial scale plant would undergone the same treatment.
- In particular the problem of the air in-leakage was the major cause of the level of the CO₂ in the flue gases lower than theoretically expected.
- Near future work: try to reduce in-leakage down to acceptable levels
- **TEA C burner**: good stable performances in oxy-RFG conditions, both with NG and coal (*no primary oxygen*)



Conclusions (2)

- The influences of the recycle ratio on the NO_x emission both in NG and coal oxy combustion were studied.
- The *in-flame* data collected during the campaigns are to be published in an IFRF report, and may be used to develop a better understanding of the changes in the chemical and physical processes involved in this kind of combustion. *Overall and In-flame measurements provide good sets of data for more fundamental analysis (flame structure, NO_x , carbon in ash, etc.)*
- They can also provide modelers with a starting hint for the development of oxy-combustion flame mathematical simulation.



Acknowledgments

These results wouldn't been achieved without the help of:

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